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# Multiple Loop Heat Pipe Radiator for Variable Heat Rejection in Future Spacecraft

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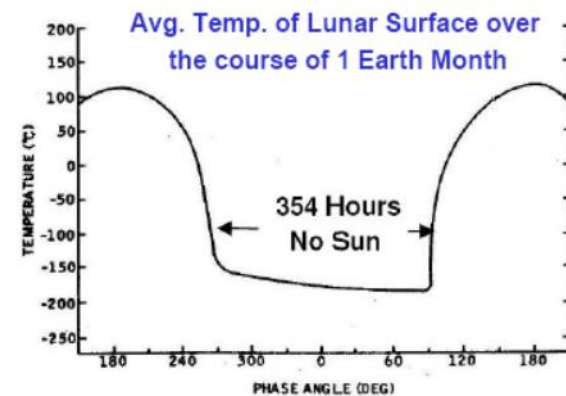
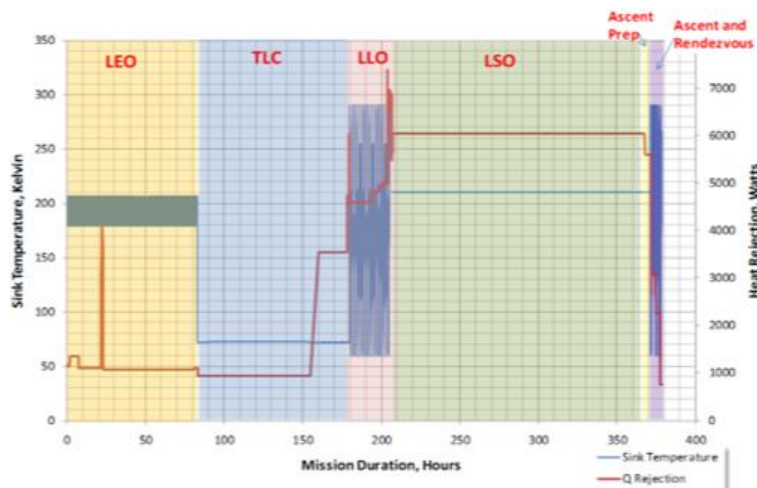
*Advanced Cooling Technologies, Inc.*



# Motivation



- Challenging space thermal environments with varying heat loads and sink temperatures will require spacecraft thermal management systems to have variable heat rejection with high turndown
  - Future manned spacecraft
  - Future Lunar and Martian rovers
- **Loop heat pipes (LHPs)** have been successfully used for variable heat rejection on spacecraft. Heat transfer with LHPs can be actively controlled through compensation chamber (CC) heating. However...
  - Heat loads practically limited to <1 kW
  - Power requirements for CC heating results in large mass penalties

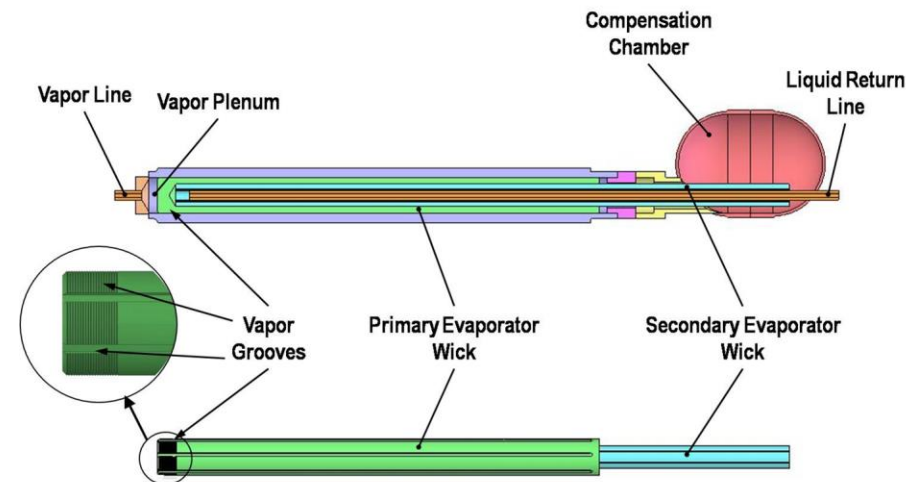
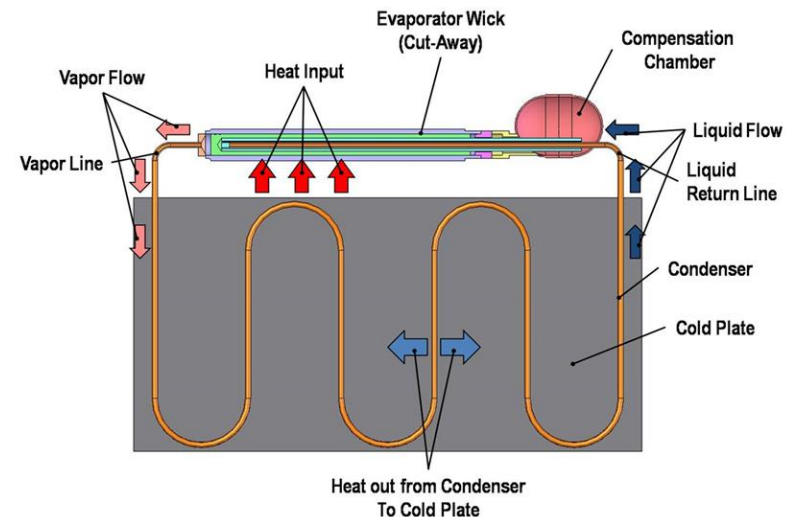




# Loop heat pipe operation



- Heat is applied to outside of **primary wick**, which is saturated with liquid
- Vapor is generated which travels through **vapor line** to **condenser**
- Vapor is condensed and the liquid sub-cooled in the condenser
- Cold liquid returns to the **compensation chamber (CC)** through **liquid line**
- CC contains saturated two-phase mixture of liquid and vapor
- CC is a lower temperature and pressure than vapor side of primary wick
- The **secondary wick** regulates liquid and vapor communication between CC and primary wick

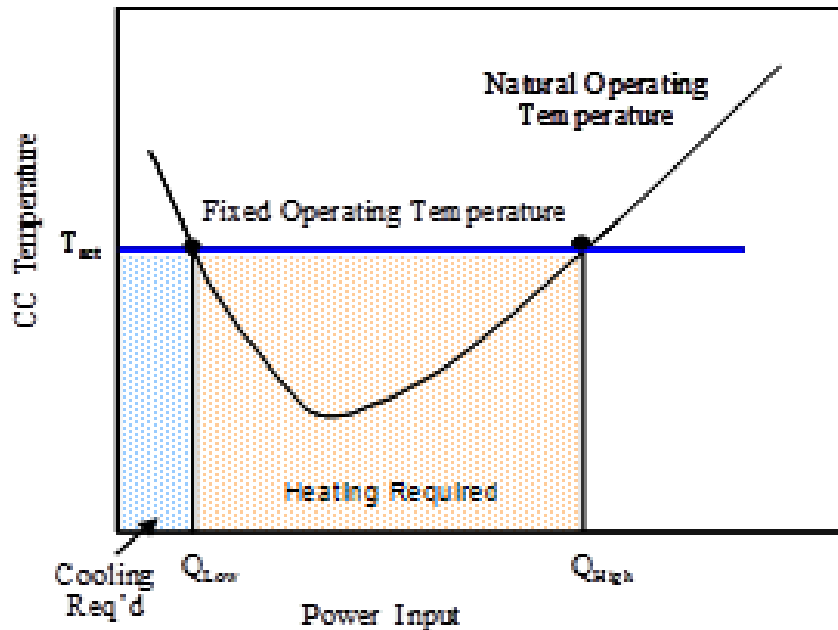




# Loop heat pipe control



- LHP evaporator operating temperature is governed by the saturation temperature in the CC
- CC saturation temperature varies with heat load and sink temperature
- Typical LHP temperature control for spacecraft is to cold bias the CC and use electrical heaters
- For a given sink temperature:



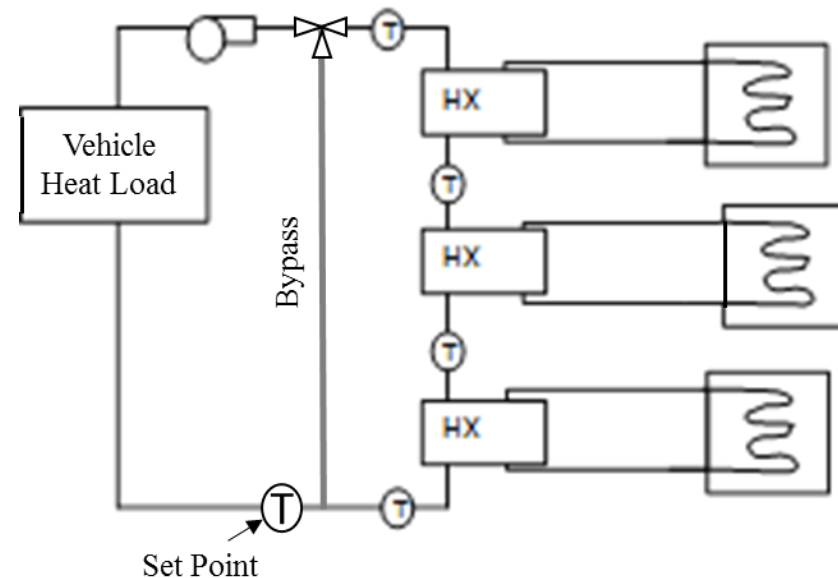
“Loop Heat Pipe Startup Behaviors”, Jentung Ku, 18<sup>th</sup> Workshop on Thermophysics in Microgravity, El Segundo, CA, March 24, 2014.

- Other methods of LHP temperature control:
  - Aluminum coupling blocks or heat exchanger between vapor and liquid lines
  - Thermoelectric devices
  - Thermal control valves for vapor bypass
  - VCHPs between evaporator and liquid line



## Multiple LHP Variable Heat Rejection System

- ACT has developed a multiple-LHP system concept for rejecting large variable heat loads (several kW) from an intermediate single-phase pumped loop that removes heat from the crew compartment of a manned spacecraft
- Goal is to maintain the set point temperature of the single phase fluid returning to the vehicle as the heat load and sink temperature changes
- **Key components of concept:**
  - LHP evaporators coupled to loop in series
  - Valve and bypass loop in single-phase loop, such that local flow rate passing through heat exchangers with LHP evaporators can be modulated
  - Changing local flow rate changes fluid temperature drop across heat exchangers, thus changing LHP evaporator temperatures, thus changing overall thermal resistance of LHP

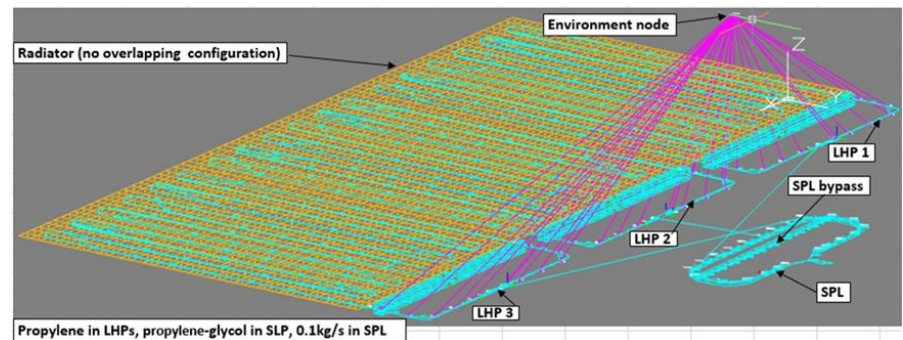
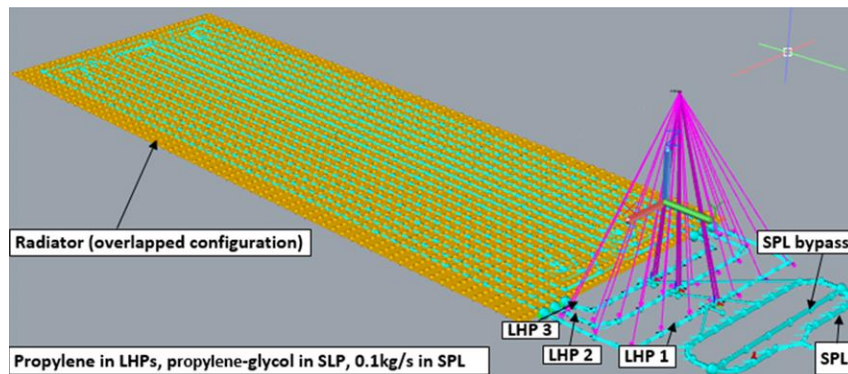




# Thermal Desktop modeling



- A systematic numerical evaluation of this concept was performed using Thermal Desktop
- Single phase fluid properties:
  - 50/50 propylene-glycol/water
  - 0.1 kg/s total mass flow rate
  - Set point temperature of 8°C
- Three LHPs, sized to reject 2500 W in warmest sink (-41°C)
  - Propylene working fluid
- Two configurations examined:
  - Separate radiator panels for each LHP
  - LHPs share common radiator panel, with overlapping condenser lines



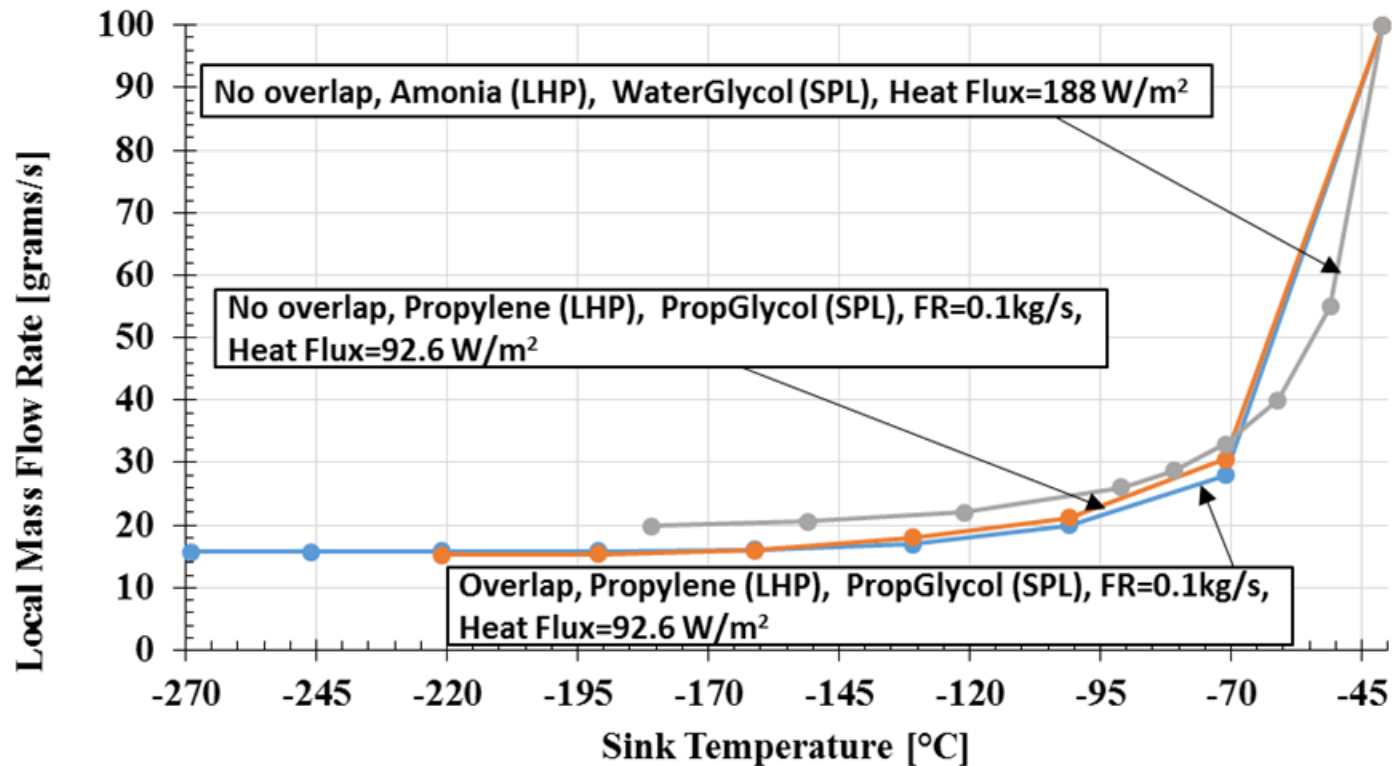




# Thermal Desktop modeling



**Constant power (2500W) into variable sink temperature**



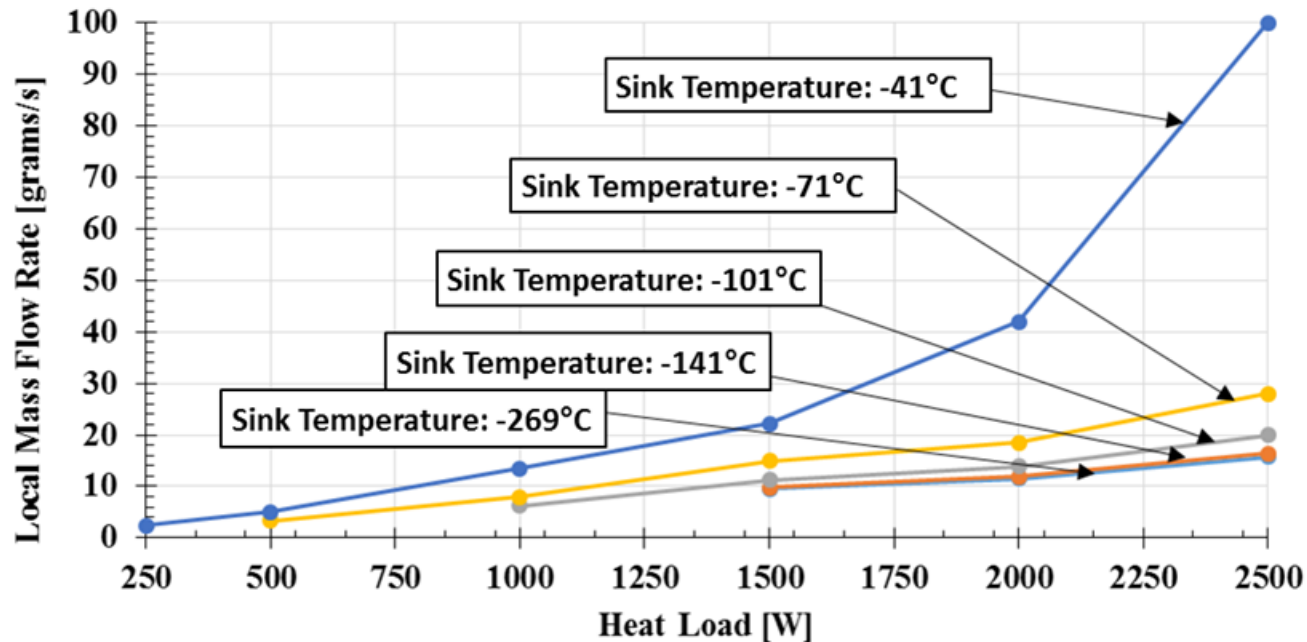
**Local Mass flow rate required to maintain set point temperature while sink temperature changes for constant power (2500W)**



# Thermal Desktop modeling



Variable power into constant sink temperature



**Local Mass flow rate required to maintain set point temperature while power changes (performed for various sink temperatures)**  
**- Results for 3 LHP with non-overlapping condenser lines**

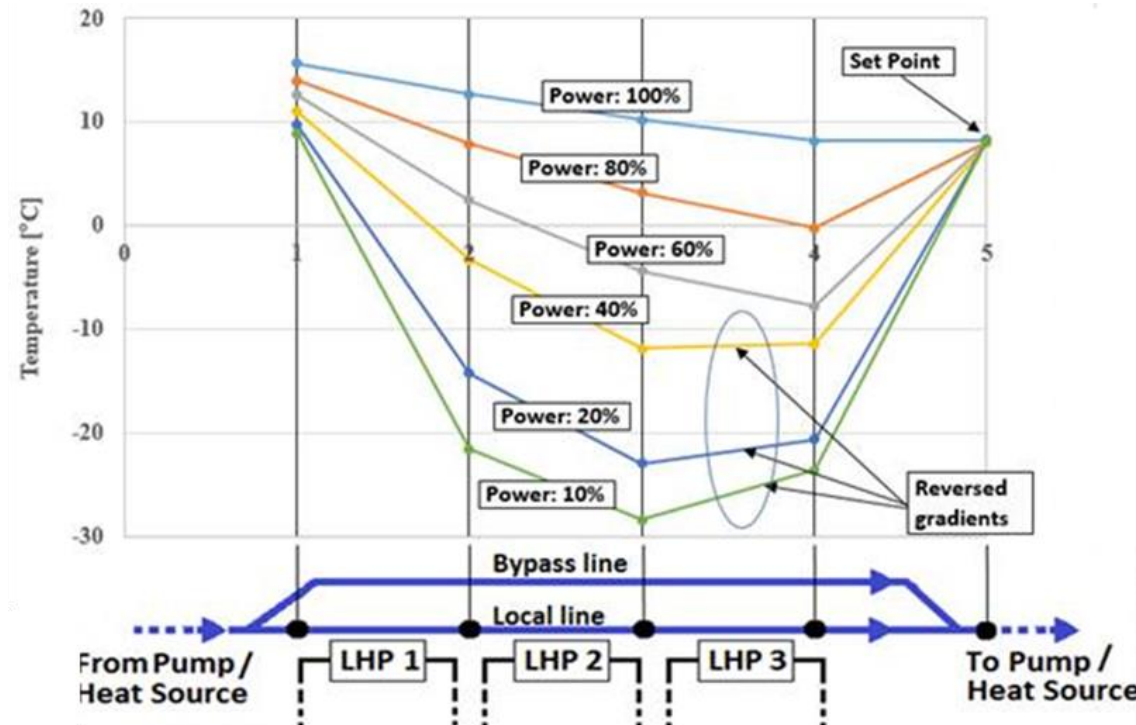




# Thermal Desktop modeling



Variable power into constant sink temperature



Temperature distribution along the local portion of the SPL as power changes for a sink temperature of  $-41^{\circ}\text{C}$

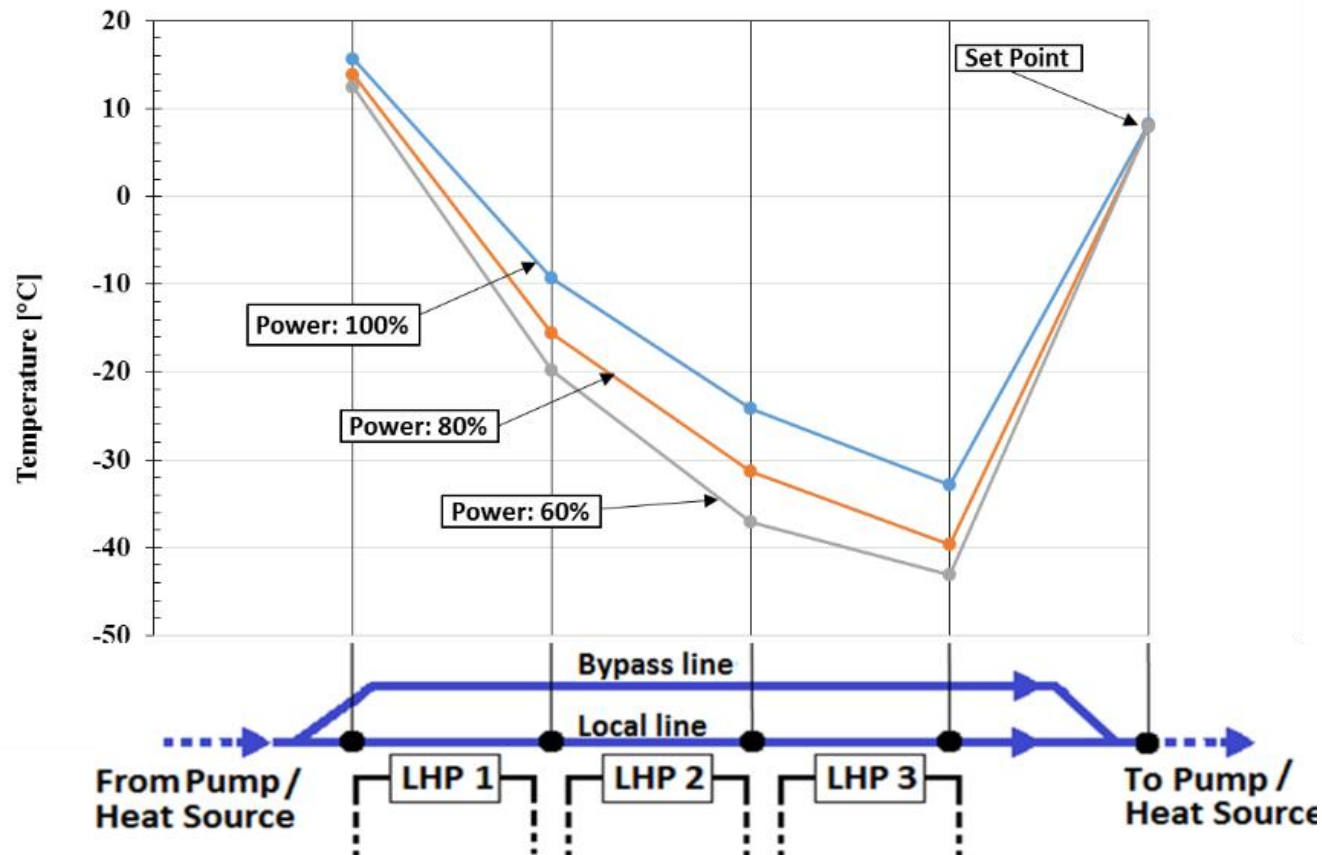
- In the cases where there is a reversed temperature gradient, the third LHP is completely shut down and loop is gaining heat from environment



# Thermal Desktop modeling



Variable power into constant sink temperature



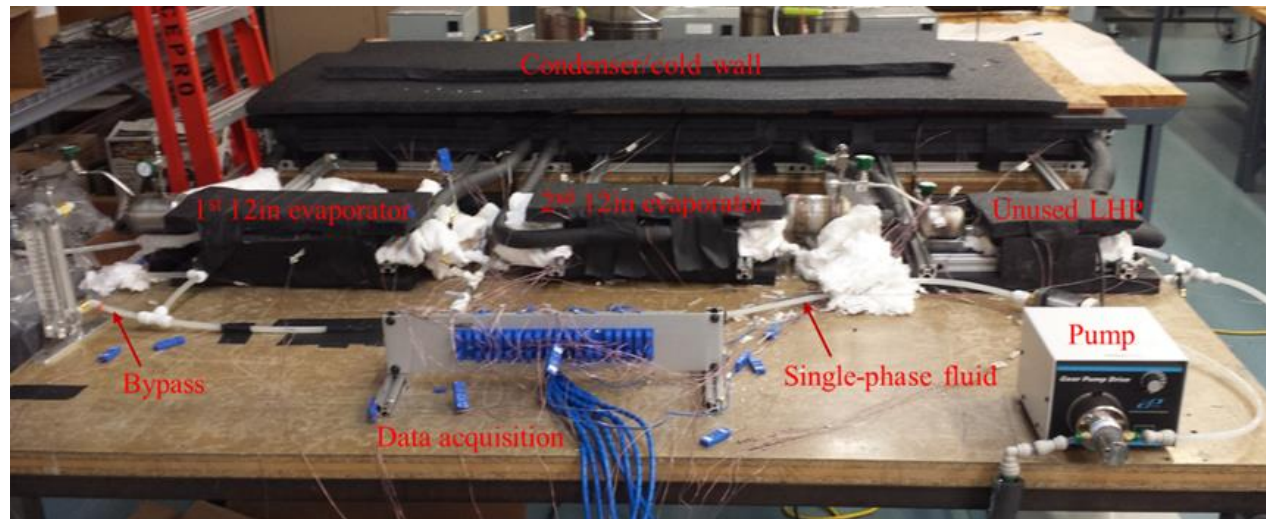
**Temperature distribution along the local portion of the SPL as power changes for a sink temperature of  $-269^{\circ}\text{C}$**



# Experimental Validation



- An experimental study was also performed to demonstrate the feasibility of the concept
- An experimental setup was constructed using existing LHPs from previous development programs at ACT
  - Test setup originally designed for 3 LHPs in series, but third LHP would not start up
  - 2 remaining LHPs: flanged evaporator coupled to pumped water loop through heat spreader plates
  - Pumped water loop configured with bypass loop to vary local water flow rate
- Due to large number of complex variables that are involved in the Thermal Desktop modeling, a direct comparison between the test setup and the model was not made
- However, a scaled down proof-of-concept system can clearly demonstrate the general conclusions of the modeling results

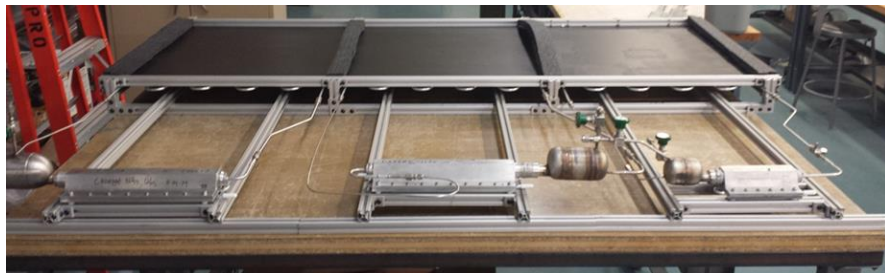




# Experimental test setup



## Variable Heat Rejection Multiple LHP test setup



**3 LHPs sharing common condenser**



First 12in evaporator



Second 12in evaporator

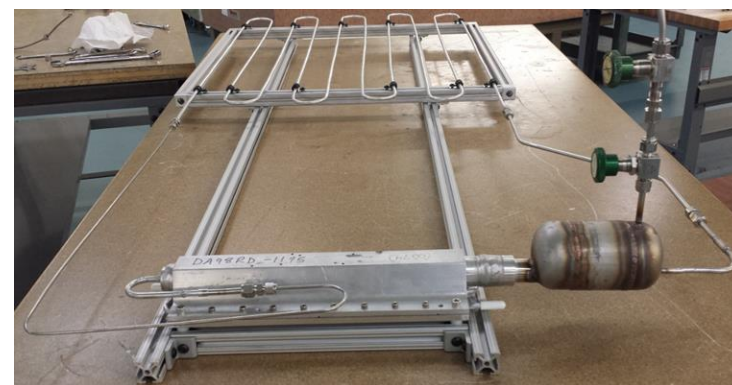


6in evaporator

**LHP evaporators used in test setup**



**Fully assembled and insulated test setup**



**Reassembled LHP using existing pump**

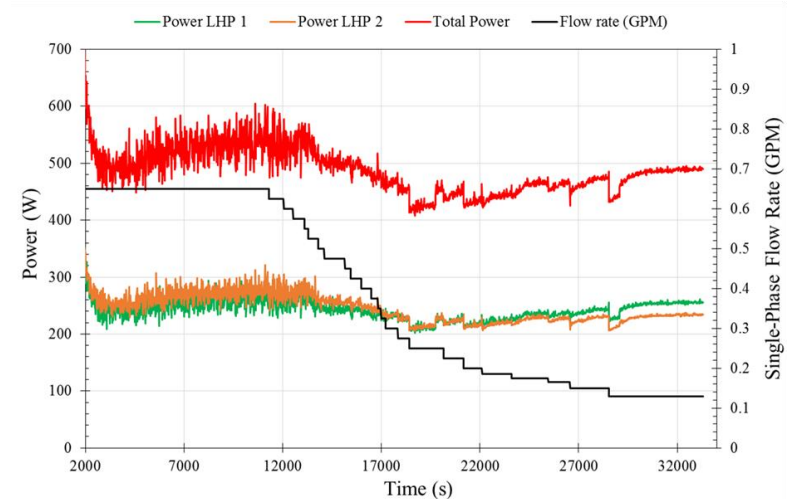
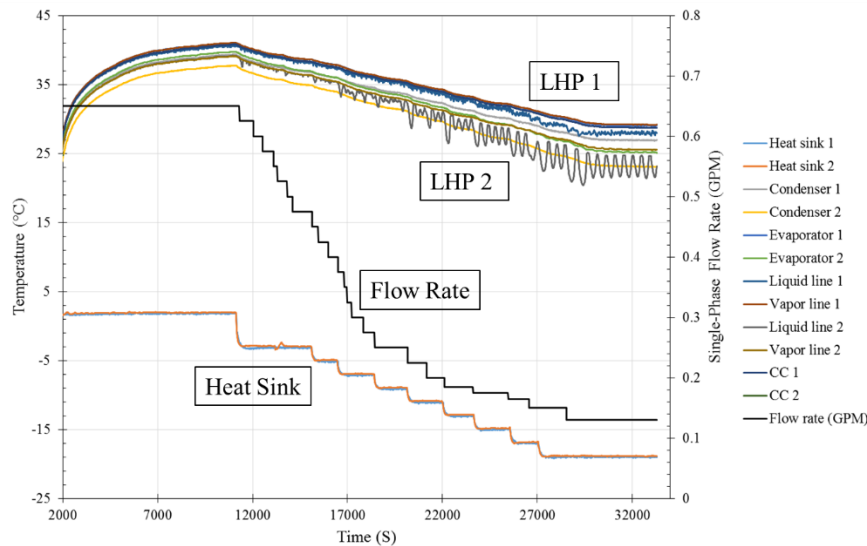
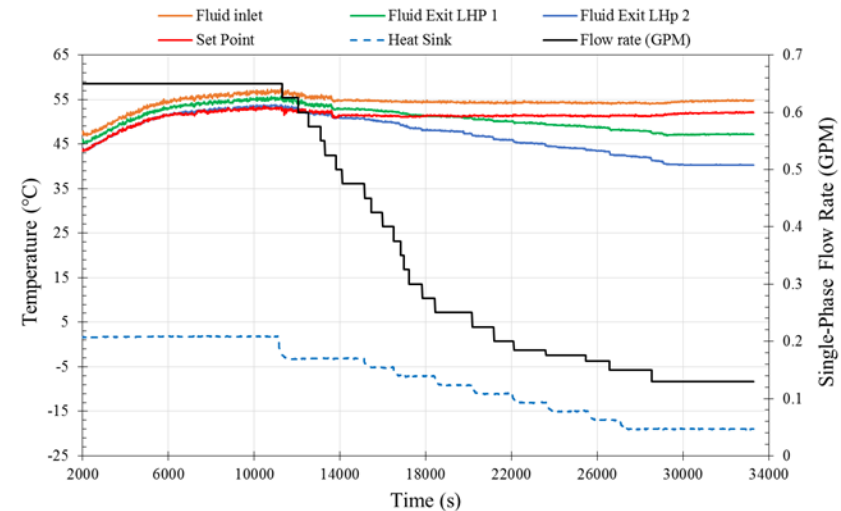




# Experimental results



- First test – variable heat sink, constant heat load
  - As heat sink temperature dropped from 2°C to -19°C, set point temperature held to within 1°C
  - Heat rejected by LHPs was fairly constant around 400-500 W
  - LHP control only through flow rate variation

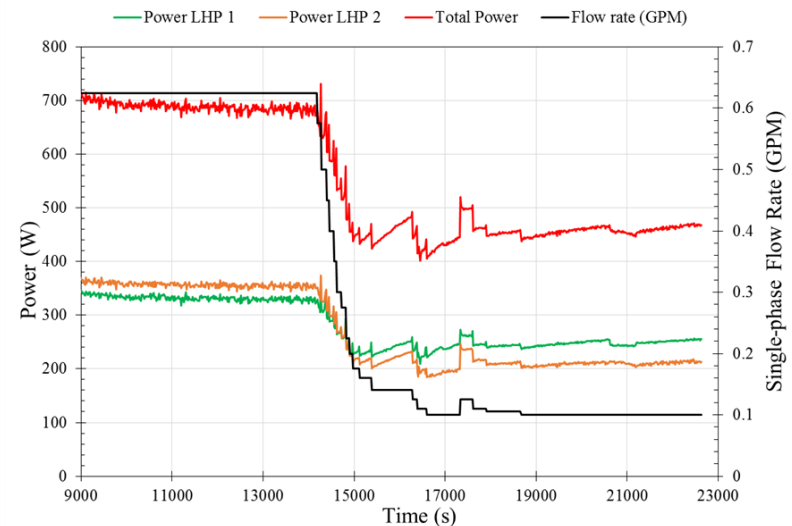
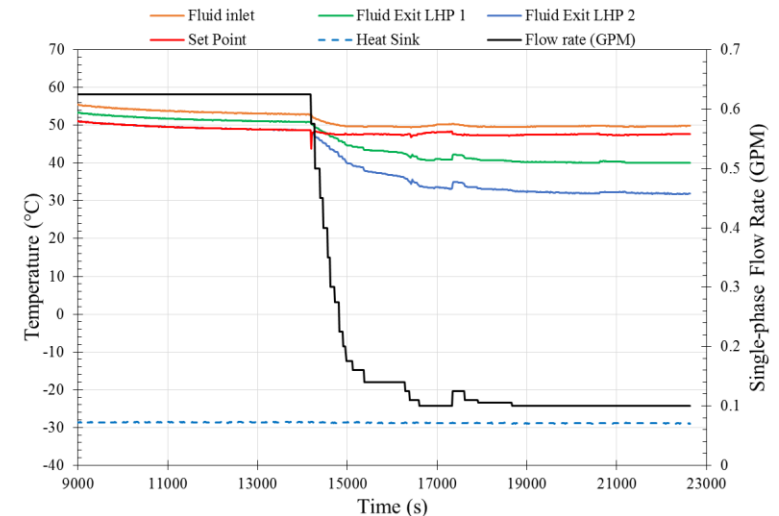
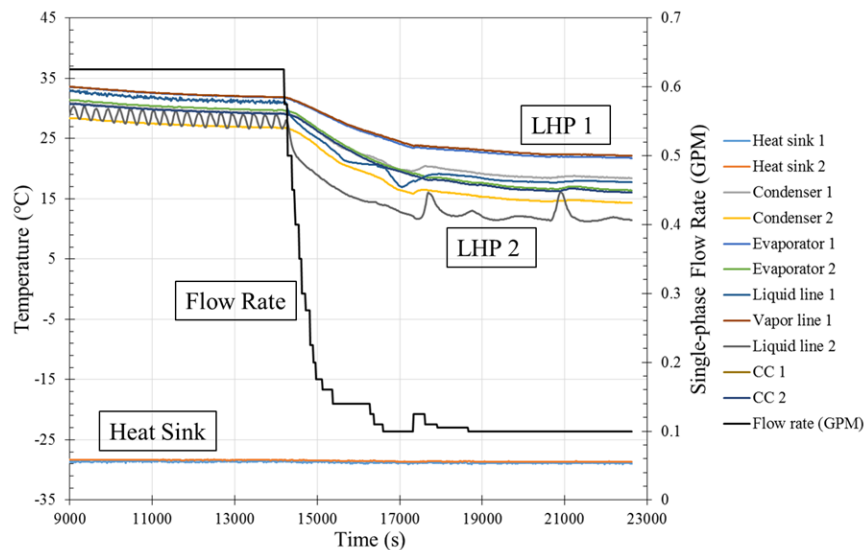




# Experimental results



- Second test – variable heat load, constant heat sink
  - For a constant heat sink temperature of  $-29^{\circ}\text{C}$ , the heat load was reduced from 700 W to 450 W – turndown of 1.5:1
  - As power was reduced, outlet set point temperature was held within  $0.5^{\circ}\text{C}$
  - LHP control only through flow rate variation







- Developed a novel method of control for a multiple-LHP system through the modulation of the local flow rate of the single-phase pumped fluid, while maintaining constant total flow rate
- Modeling effort demonstrated capability of maintaining single-phase fluid set point as sink temperature varies from  $-41^{\circ}\text{C}$  to  $-269^{\circ}\text{C}$  while rejecting 2.5 kW
- Modeling effort also demonstrated a turndown ratio of **10:1** for a 2.5 kW, 3 LHP system at sink temperatures of  $-41^{\circ}\text{C}$  and a turndown ratio of 1.5:1 for the same system at sink temperatures of  $-269^{\circ}\text{C}$
- Flow rate based control was demonstrated experimentally with a 2 LHP system for both cases, validating the numerical results
  - Varying sink, constant heat load – maintained set point as sink temperature dropped  $20^{\circ}\text{C}$
  - Varying heat load, constant sink – demonstrated turndown ratio of 1.5:1



## Acknowledgments

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